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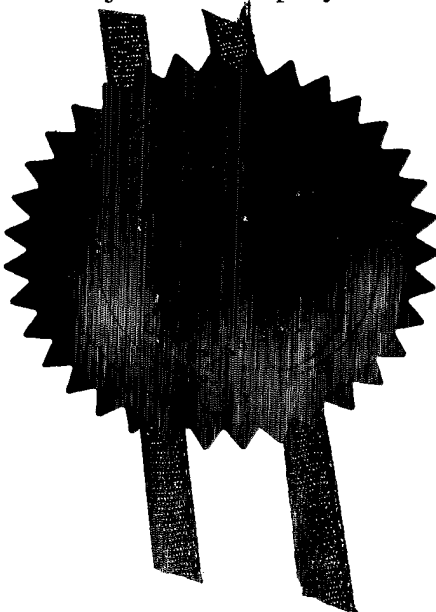
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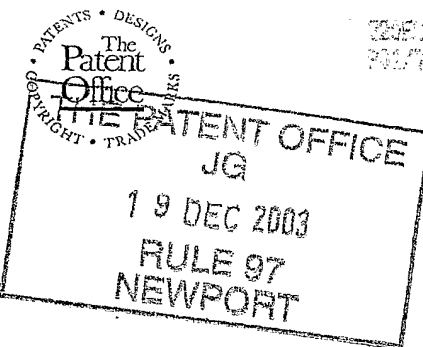
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1. Your reference P3190 GB PRO
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2. Patent application number
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3. Full name, address and postcode of the or of each applicant (*underline all surnames*)
Nuground Limited
Nanotechnology Centre
Herschel Building, Newcastle University
NEWCASTLE UPON TYNE, NE1 7RU

Patents ADP number (*if you know it*)

If the applicant is a corporate body, give the country/state of its incorporation

United Kingdom

872608001

4. Title of the invention Waste Dewatering Treatment System and Method

5. Name of your agent (*if you have one*) NOVAGRAAF PATENTS LIMITED

"Address for service" in the United Kingdom to which all correspondence should be sent (*including the postcode*)

THE CRESCENT
54 BLOSSOM STREET
YORK YO24 1AP

Patents ADP number (*if you know it*) 08299166001

6. Priority: Complete this section if you are declaring priority from one or more earlier patent applications, filed in the last 12 months.	Country	Priority application number (<i>if you know it</i>)	Date of filing (<i>day / month / year</i>)
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7. Divisionals, etc: Complete this section only if this application is a divisional application or resulted from an entitlement dispute (see note f)	Number of earlier UK application	Date of filing (<i>day / month / year</i>)
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8. Is a Patents Form 7/77 (Statement of inventorship and of right to grant of a patent) required in support of this request? Yes

Answer YES if:

- a) any applicant named in part 3 is not an inventor, or
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Continuation sheets of this form

Description

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Claim(s)

Abstract

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Priority documents

Translations of priority documents

Statement of inventorship and right to grant of a patent (Patents Form 7/77)

2

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11. I/We request the grant of a patent on the basis of this application.

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NOVAGRAAF PATENTS LIMITED

Date 18/12/2003

12. Name, daytime telephone number and e-mail address, if any, of person to contact in the United Kingdom

Peter Wilson (Dr)

01904 610586

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WASTE DEWATERING TREATMENT SYSTEM AND METHOD

5 The invention relates to a system and method for the treatment of industrial wastes comprising a dispersion or suspension of solid particles, more particularly inorganic particles being a byproduct of mining, manufacturing or other industrial processes, in a liquid. The invention relates to a system and method to reduce the liquid content thereof. In particular the invention relates to a system and method for the dewatering of mine tailings and the like.

10

Industrial wastes are the by-products of construction, mining or manufacturing processes. They possess both physical and chemical properties, which can interact with the natural or artificial ecosystems that they occupy.

15 Tailings wastes deposited in dams represent some of the largest man-made structures in the world. The large quantities of water stored in the voids of these tailings impoundments can make them potentially unstable and a potential risk to underlying ground water. Many tailings disposal facilities contain material that undergoes extremely slow self-weight consolidation.
20 Examples include the fine tailings produced in the Oil Sands industry, and the waste products from the phosphate mining industry.

Social, legal and financial pressures are being directed towards the problems arising from industrial wastes. For example, in the United Kingdom the
25 Special Waste Regulations (1996) SI 1996/972 are to be replaced by the Hazardous Wastes Regulations in 2003/4 and the Landfill (England and Wales) Regulations (2002) SI 2002/1559 are soon to be enacted. These changes are likely to result in an increase in the cost of disposal of industrial wastes.

One approach to the waste problem is waste minimization. This can be achieved by reclamation, recycling or by volume reduction. It is apparent that these types of materials can be reduced significantly in volume if the solid content can be increased by dewatering. Mechanical methods alone are not necessarily effective over practical timescales. A known method to achieve more rapid dewatering in principle is by the use of electrokinetic processes, which remove or reduce the water content of the waste resulting in a significant overall reduction in the quantity of material that needs to be disposed of.

Electrophoresis dewatering

Many waste materials (tailings) include a significant proportion of particles that are finer than $20\mu\text{m}$ size. It is these particles which make electrophoresis dewatering possible as they usually have an electrically charged surface, most commonly a negative charge. Surrounding the charged particle is a double layer of cations, the concentration of which decreases with distance from the surface of the particle. Application of an electrical current to such a material causes movement of the ions. The charged particles will move towards the anode if negatively charged and towards the cathode if positively charged. This factor alone may not be the only reason that electrophoresis may be successful in clarifying water containing a suspension of fine material (tailings); changes in pH can also exert a major influence on the settling characteristics of clay particles.

Electrokinetic Dewatering

Electrokinetic dewatering of materials relates to the movement of electrically charged particles known as electrophoresis, and the movement of water through a matrix of solid particles usually referred to as electro-osmosis. Both phenomena occur under the application of a direct (DC) electrical current. Electrophoresis deals with slurries or suspensions having a very low solids content, and electrosmosis can be used to treat mixtures and materials that have undergone some consolidation and where the solid particles are in contact with one another forming a discrete matrix or skeleton.

The strength of an electrical charge on a clay particle, or its degree of electronegativity, is often quantified in terms of its zeta potential. The zeta potential is usually defined as the electrical potential at the junction between the fixed and mobile parts of the electrical double layer. It is dependent on the pH of the surrounding liquid and is also influenced by the valence of the ions present in a waste. As the association between clay surfaces and high valence cations increases, the zeta potential decreases. In some cases electrophoresis dewatering commences at 1V DC; with calcium clays dewatering may start between 5.5-10V DC and in the case of aluminium wastes 25V DC may need to be applied to start the process.

Electro-osmotic dewatering

It is established that the application of an electrical field across a soil sample results in the attraction of cations to the cathode and anions to the anode. As these ions migrate they drag their water of hydration with them resulting in a force on interstitial water that causes free water to migrate to one of the electrodes. As most clay soils tend to be negatively charged and thus

surrounded by an outer cloud of positively charged water molecules, water migrates towards the cathode during electro-osmotic dewatering. The rate of this water movement is *independent* of the pore size of the soil and depends upon the applied voltage gradient and certain characteristics of the parent material. The independence of electro-osmosis dewatering with respect to pore size means that the technique is effective in fine-grained soils.

The field applications of electro-osmosis frequently relate to accelerated consolidation and strength gain in natural clay soils. As many industrial wastes are derived from clay minerals it is postulated that the technology can be applied to their treatment, particularly where dewatering is the basis of the improvement.

Difficulties of Electro-kinetic dewatering of Wastes

15

The application of electro-kinetics to the treatment of wastes has been limited in particular by problems associated with the nature and form of available electrodes. Metal electrodes corrode causing degradation of the electro kinetic process, changes to the chemistry and potential contamination. Non-metallic systems have not been practical on an industrial scale. Accordingly, although the theoretical basis for application of electro-kinetics to the treatment of wastes to reduce volume by dewatering is established, the practical application of systems and methods based on this has been limited to specialist situations and has not been successfully applied generally on an industrial scale

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It is an object of the present invention to mitigate some or all of the above limitations.

It is a particular object of the present invention to provide an apparatus and method for the removal of liquid from industrial wastes comprising a dispersion or suspension of particles in a liquid, more particularly inorganic particles being a byproduct of mining, manufacturing or other industrial processes, which applies eletro-kinetic principles but is more practically applied to a range of wastes on an industrial scale than has been possible to date.

It is a particular object of the present invention to provide an apparatus and method for the removal of liquid from such industrial wastes offering enhanced speed and/ or efficiency and/or extent of liquid removal.

Thus according to the invention in a first aspect there is provided an apparatus for reducing the liquid content of a material comprising a particulate/liquid dispersion or suspension, and in particular comprising a dispersion or suspension of inorganic particles being a byproduct of mining, manufacturing or other industrial processes, the apparatus comprising a receiving zone to contain the material, at least one pair of electrodes spaced apart within the receiving zone, means to apply a potential difference thereacross and hence across the material in use to drive electro-kinetic dewatering, and drainage means to enable removal of water, wherein at least one of the electrodes (in use the cathode) comprises a textile or other synthetic material at least in part associated with a conductor so as to constitute where so associated a conducting electrokinetic textile or other synthetic material.

25

The first electrokinetic textile or other synthetic electrode acts with the second remotely spaced electrode in contact with the material to allow application of a potential difference across the material to be treated in the receiving zone. This enables an electrokinetic dewatering process to be driven. The drain

draws off water at the cathode, and the material is dewatered, and so consolidated and reduced in volume.

The general chemistry is as above described. However, the novel use of the electrode material within the process overcomes many of the problems of prior art metal electrode systems. Materials in accordance with the invention can be made resistant to corrosion, and so do not adversely affect the electrochemistry of the system in use. They can readily be formed in a range of shapes. Further, they can combine the established geosynthetic functions of filtration, drainage and reinforcement as well as being electrically conductive. Such materials are found to be surprisingly and usually effective, not merely as an alternative to metal electrode systems, but as an element, even though the mode of action differs from that in the conventional application of such materials in the consolidation of soil structures.

15

The apparatus or method of the invention may provide for a separate drain. However, this last feature can be exploited in a preferred embodiment in that the drain is provided in close association with, and in particular formed as an integral structure with, the conducting electrokinetic textile or other synthetic material electrode. In a particular example of this, the receiving zone is at least partly defined by a filtration membrane permeable to the liquid but impermeable to at least some and more preferably substantially all of the particulate solids contained within the material, which filtration membrane comprises a textile or other synthetic material at least in part associated with a conductor so as to constitute where so associated the said conducting electrokinetic textile or other synthetic electrode.

25

The electrokinetic textile thus combines a role as an electrode driving the electrokinetic enhancement of the dewatering process with a means of acting

as a drainage/filter medium in a conventional filtration membrane role. It will be apparent that many of these advantages will also be relevant to the second electrode. According in a preferred embodiment, the second electrode is also a conducting electrokinetic textile or other synthetic material.

5

The filter membrane used in the apparatus or method is described as a textile or synthetic which in this context means a sheet-like material having a primarily polymeric base structure. The textile may be woven, knitted, needle-punched, non-woven or otherwise fabricated. The textile may include
10 conducting elements, which may be metallic, in a composite material composition, but is critically not fabricated entirely or primarily from metal alone. Particularly suitable materials will include those materials known for use as conducting geosynthetic materials.

15

A key to the apparatus or method of the invention especially in its preferred embodiment is that the textile or like synthetic material is able in use to function, at least over a part of the area thereof, as an electrokinetic textile/synthetic material. It will be apparent that this can be achieved in two ways.

20

First, it can be effected by provision of a separate conductor so disposed within the apparatus as to be caused during use to come into contact with the filtration membrane material over at least a part of the area thereof. In the alternative, it will in many instances be more convenient if the electrode is at
25 least partly comprised of a conductor, either in that the material is inherently conducting or in that it integrally incorporates conductive material into its structure.

In the preferred embodiment the electrode also serves as a filtration membrane. In such a case the entire filtration membrane may integrally comprise conducting electrokinetic textile/synthetic material. Conveniently however, the filtration membrane preferably comprises a plurality of discrete
5 conductive regions. This allows applied current in use to be limited to discrete areas within a receiving zone as required.

The electrodes provided for use in accordance with the apparatus or method invention do not corrode as readily as conventional electrodes. Previous
10 attempts at introducing electrokinetic processes to industrial dewatering technology have frequently failed due to the rapid deterioration of the electrodes through corrosion and due to the electrochemical effect of this corrosion on the process. By contrast, there is a body of established technology, particularly in relation to electro-kinetic geosynthetic materials,
15 which will provide materials able to resist environmental degradation. In accordance with the invention, these materials are found to be surprisingly effective when applied to the dewatering of some industrial wastes. In the preferred case therefore, an electrokinetic geosynthetic material is used. This can provide all the functions of a conventional geosynthetic material (in
20 particular an integral drainage and filtration function) as well as acting as an electrode. The results are positive although, whilst the invention is not limited by any theory of operation, it would appear as described with reference to the detailed examples below that the mode of action is surprisingly different to the mechanisms associated with their prior art uses in the consolidation of natural
25 soils.

The principles of conducting electrokinetic geosynthetic materials have been established, and were for example set out in International Patent application number WO95/21965 to Jones *et al* incorporated herein by reference.

The EKG material of the electrode may have any suitable composition to give conductive properties. For example, the conductive geosynthetic material may comprise a generally inherently non-conductive geosynthetic material in association with at least one metallic or non-metallic conducting element to produce a composite conducting geosynthetic material. Alternatively, the geosynthetic material may be inherently conducting, for example being loaded with conducting particles, and for example comprising polymeric material loaded with carbon. Such inherently conducting geosynthetic material may additionally be associated with at least one separate metallic or non-metallic conducting element, to provide a composite conducting geosynthetic.

In a preferred embodiment, the electrokinetic material (EKG) comprises a woven or non-woven polymeric and for example geosynthetic material incorporating a plurality of elongate conducting elements therewithin, in particular in one or more parallel arrays. The conducting elements may for example be threaded through or woven into the basic geosynthetic material. Two or more arrays may be disposed in different directions to form a network structure. Where the EKG comprises also a filtration membrane this will generally comprise sheet material, and the elongate conducting elements will be disposed generally laterally therewithin.

A possible electrically conducting geosynthetic material could simply comprise a conventional geosynthetic material which has woven therein, or threaded therethrough, electrically conducting filaments or threads which may be single or multi-stranded. The filaments or threads comprise conducting elements. In the instance where the electrically conducting geosynthetic is woven, electrically conducting threads or filaments may be intertwined with or enmeshed within conventional geosynthetic materials and in the instance

where the electrically conducting geosynthetic is provided in a threaded form any preselected number of passages of thread through the material may be made according to a user's requirement.

- 5 The ability of electrokinetic phenomena to move water, charged particles and free ions through fine-grained low permeability substrate is established. There are five principal electrokinetic phenomena: streaming potential, migration potential, electro-osmosis, ion migration and electrophoresis. The last three are concerned with the transport mechanisms developed upon application of an electrical field across a substrate mass and are relevant to the present invention, which exploits electro-osmosis in particular.

To generate an electro-osmotic effect, an electrical field is applied across a mass of material in the receiving zone. Cations are attracted to the cathode and anions to the anode. The transport mechanism is as explained above. In order to maintain a charge neutrality, there are more cations than anions in the pore fluid of the substrate containing negatively charged particles. Therefore there is usually a net flow of water to the cathode. This electro-osmotic flow depends upon the applied voltage gradient and the electro-osmotic permeability of the material.

In accordance with the invention, the electro-kinetically induced drainage enhances the liquid removal process. For a given material, advantages can be obtained both relating to the speed at which liquid is removed and relating to the maximum degree of drying which can be practically obtained.

The receiving zone may comprise a real, closed containment means into which waste material may be fed for batch processing, or may comprise a treatment zone in an unclosed, semi-contained, continuous processing system. For

example it may comprise containment means defining a conduit with an untreated material input, a treated material output remote therefrom, and a treatment zone therewithin. In either case, the containment means preferably comprises at least in part a filtration membrane being associated with a conductor for at least a part of the extent thereof to serve as a combined electrode and filter/ drain in the manner above described.

Where it is desired to apply a potential difference across the material in a region relating to only a part of such a filtration membrane, this may be achieved in that a conductor is associated only with that part of the filtration membrane. Alternatively, conductors may be associated with the membrane across substantially its entire area, for example in a plurality of discrete regions, but only electrically supplied in the desired region. Where the membrane comprises EKG material, the latter approach may be preferred.

It will be understood that none of the foregoing requires the area associated with the conductor or the second electrode to be continuous in the region where a potential difference is to be applied. Either or both may instead be disposed as a discontinuous plural array provided that the arrangement permits the application of the necessary potential difference across the material to be dewatered to generate the necessary electrokinetic effect.

In accordance with the invention in a further aspect there is provided a method of reducing the liquid content of a material comprising a particulate/liquid dispersion or suspension, and in particular comprising a dispersion or suspension of inorganic particles being a byproduct of mining, manufacturing or other industrial processes, the method comprising receiving untreated material in a receiving zone; providing at least one pair of electrodes spaced apart within the receiving zone, at least one of which (in use the cathode)

comprises a textile or other synthetic material at least in part associated with a conductor so as to constitute where so associated a conducting electrokinetic textile or other synthetic material electrode; applying a potential difference thereacross and hence across the material to drive electro-kinetic dewatering;
5 removing water thus driven to the cathode by suitable drainage means.

The method may be a batch process, in which case the treated material is then simply removed from the receiving zone. Alternatively, the method is a continuous process, wherein the receiving zone comprises a treatment zone in
10 a conduit between an input and an output thereof, and the method comprises feeding untreated material into the input, causing the material to travel therealong through the treatment zone where the above dewatering method is applied, and removing the treated material at the output.

In particular the method is a method for the treatment of inorganic mining or
15 industrial waste and especially mine tailings by dewatering.

The invention will now be described by way of example only with reference to figures 1 to 3, representing experimental data for dewatering employing the principles of the invention.

20

Example 1: Accelerated sedimentation of suspended diamond tailings (Electrophoresis)

The material treated was obtained from a diamond mine tailings
25 impoundment. A feature of the waste was that it contained extremely fine clay particles which do not settle out, resulting in the decant water having such a high suspended solids content (1 to 2%) that it cannot be reused in the metallurgical plant, nor can it be released into a water course. Previous efforts to clarify the water by adding lime and organic flocculants were unsuccessful

and all the water has to be retained in an impoundment. This is an uneconomic use of space, which could better be used to store tailings solids.

The dominant mineral in the tailings waste, determined by X-ray diffraction was montmorillonite, the Plasticity Index (PI) was 38 and the percentage of material finer than $2\mu\text{m}$ was 41%. The pH of the tailings water ranged between 8.9 and 9.0. The ambient pH of around 9 corresponds to the region of most negative zeta potential. The suspension remained stable at this pH as the repulsive forces are at their maximum. Altering the pH, by the addition of an acidic solution could eventually reduce the repulsive forces sufficiently to enable agglomeration of suspended particles to occur. The costs of this approach are high and electrophoresis offers an alternative solution.

In the tests, two EKG electrodes in the form of an electrical Prefabricated Drain (e-PVD) were suspended vertically in a container containing a sample of the tailings. A separate control container was located next to the experimental container to provide quantification of evaporation losses. A voltage of 10V with a 1.15Amp current was applied at the start of the test. During the experiment the pH at the anode, cathode and centre of the test cell was measured together with the current drawn. The volume of water lost to evaporation was determined. The tests were repeated at potentials of 20V and 30V.

Figure 1 shows that the pH *rose* steadily as each test progressed, with a more rapid rise being apparent for voltages of 20V and 30V. The ubiquitous rise in pH is different to what usually occurs near to a metallic anode, where a *drop* in pH is usually observed; this is due to the alternate anode reaction that occurs with an EKG electrode, namely electrolysis.

The turbidity of the solution did not change until a pH value of approximately 10.5 was reached, after which the solution cleared rapidly, with the solid particles settling out within a matter of hours. Settlement of the fine particles corresponded to the point at which the zeta potential became less negative.

- 5 This was confirmed in settling tests undertaken in measuring cylinders in which the pH solution was adjusted by the addition of either sodium hydroxide or hydrochloric acid to raise or lower the pH respectively.

Example 2: Accelerated consolidation of tailings slurries

10 (Electro-osmosis)

The potential for electro-osmotic consolidation of mine tailings has been investigated using an electro-osmotic cell. The materials tested were a mineral sands tailings and diamond tailings

15

- The results of the tests are shown in Figures 2 and 3. The results are provided in terms of the degree of consolidation versus time for the two tailings under an applied vertical total stress of 25kPa. The results relate to the first one hundred minutes of testing, as this emphasizes the significance of the electro-
- 20 osmotic effect. The amount of final settlement of the tailings specimens was similar (about 5% more in the electro-osmosis test), but the rates of consolidation of the electrically treated material were significantly different to the control materials, particularly in the early stages of a test. It is difficult, if not meaningless, to calculate conventional coefficients of consolidation (c_v)
- 25 values for the electro-osmotic tests because the time-settlement curves differ so markedly from classical soil mechanic consolidation curves. In particular, it was unexpectedly found that for the diamond mine tailings approximately 50% of the total consolidation settlement occurred within one minute of the start of the test. In the case of the mineral sands 19% of the consolidation

occurred within one minute and 40% after 100 minutes. Following this very rapid period of electrically induced consolidation, the time vs. degree of consolidation curves become approximately linear until final settlement was reached.

5

The main benefit in using electro-osmotic treatment using EKG electrodes is not so much the amount of final settlement achieved, but rather the speed with which the settlement is achieved, that is so impressive. Considering that up to 50% of the final settlement occurred in about a minute, it may be that the application of an electro-kinetic force is only required for a short period and then natural self-weight consolidation may be used. In this second stage the primary function of the EKG would be to filter fine particles, allowing only clean process water to enter the EKG, which would preferably be formed as an e-PVD.

10
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Example 3: Application of EKG Materials to Tailings Dewatering

EKG materials can be formed as linear elements such as e-PVD wick drains or tapes, or in 2-dimensional forms such as belts or sheets. In continuous processes, the use of electrically conductive belts may be preferred. With batch processes, e-PVD wick drains are likely to provide an optimum configuration as, following the electro-kinetic phase, the filtration and drainage properties of the material can be utilized.

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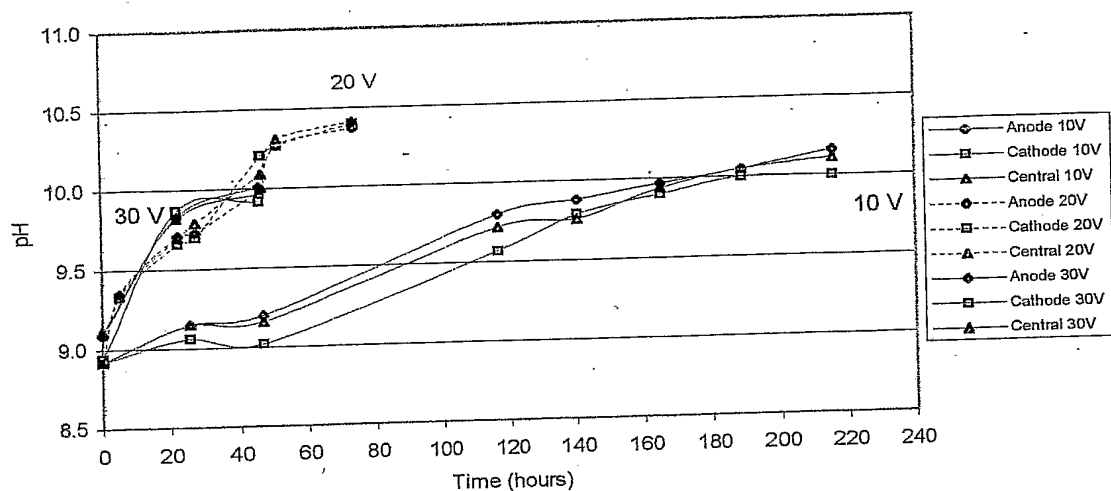


Figure 1 Change of pH with time for diamond tailings suspension tested at different voltages

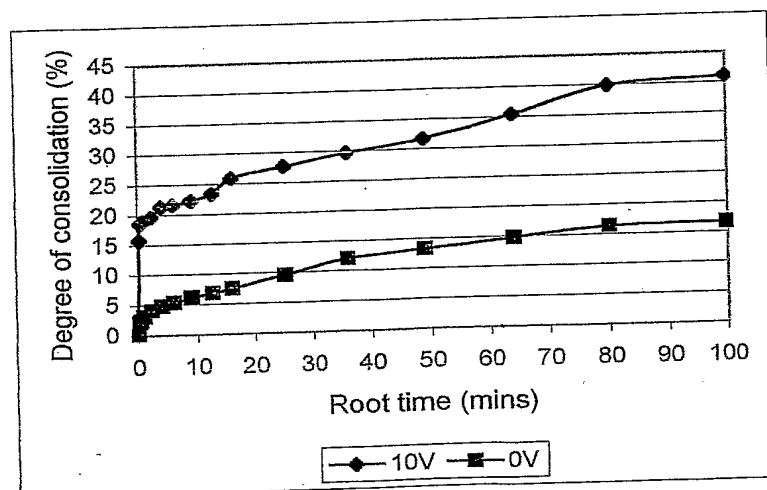


Figure 2 Variation of degree of consolidation with time for mineral sands tailings



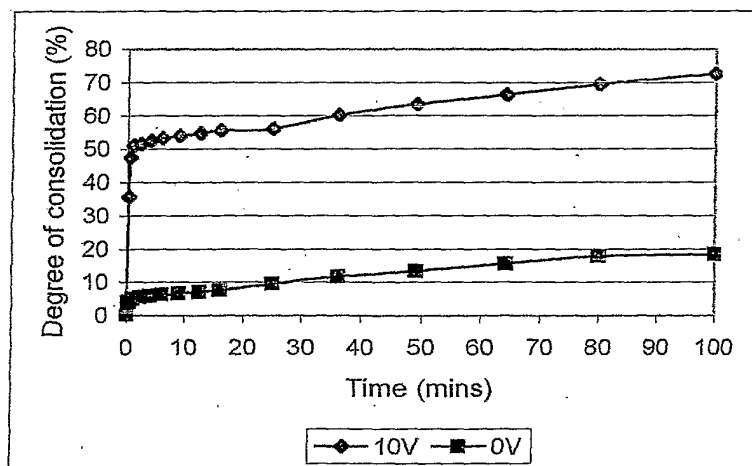


Figure 3 Variation of degree of consolidation with time for diamond tailings

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